

# Combustion synthesis of ferromagnetic Al<sub>2</sub>O<sub>3</sub>-based cermets in thermal explosion mode

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Received: 20 January 2010 / Accepted: 28 May 2010 / Published online: 8 June 2010  
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**Abstract** The ferromagnetic Al<sub>2</sub>O<sub>3</sub>-based cermets with different ratios of Co and Co–50Ni alloys were successfully prepared by combustion synthesis in thermal explosion (TE) mode. The reaction process, microstructure, and magnetic property of cermets were investigated. The relative density of cermets can be over 95% via uniaxial loading at the time of ignition when the cermets are hot and ductile. In Al<sub>2</sub>O<sub>3</sub>–Co cermets, β-Co and α-Co co-exist at room temperature with average size of less than 10 μm and disperse homogeneously in the matrix, while in Al<sub>2</sub>O<sub>3</sub>–(Co–50Ni) cermets, the network-like Co–50Ni alloy can infiltrate into the boundary gaps of Al<sub>2</sub>O<sub>3</sub> particles. The ferromagnetic Co and Co–50Ni alloys are responsible of the magnetic properties of Al<sub>2</sub>O<sub>3</sub>-based cermets. The saturation magnetization strongly depends on the magnetic characteristics and ratios of ferromagnetic phases. Al<sub>2</sub>O<sub>3</sub>–(Co–50Ni) cermets have soft magnetic properties with high magnetic susceptibility and low coercive force.

## Introduction

Al<sub>2</sub>O<sub>3</sub>-based cermets reinforced with nano- and sub-micron-scale metal particles have been studied as structural materials over the past decades [1–3]. Recently, the ferromagnetic Al<sub>2</sub>O<sub>3</sub>-based cermets, which have homogeneously dispersed ferromagnetic metal or alloy particles in Al<sub>2</sub>O<sub>3</sub> matrix, such as Fe, Co, and Ni, are very attractive because on the premise of improving the toughness of

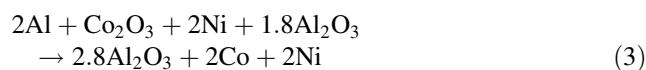
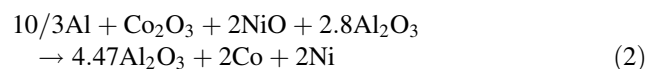
monolithic Al<sub>2</sub>O<sub>3</sub> ceramic, magnetic properties can be introduced into structural materials [4–6].

Comparing with conventional preparing process for ferromagnetic Al<sub>2</sub>O<sub>3</sub>-based cermets, such as hot pressing [7] and high-energy ball milling [8], combustion synthesis which takes advantage of the self-sustained high exothermic reaction of reactants is proved to have particular superiority for preparing composites, such as high purity of products, simple processing facilities, low costs of process, and formation of new metastable phases [9]. However, the combustion synthesized products always represent high porosity which is mainly responsible for its inferior mechanical properties and limits the application of products as structural materials. It has been demonstrated that application of pressure during or after the combustion step can considerably increase the product density [10]. Therefore, we use combustion synthesis combined with densification technique to efficiently prepare ferromagnetic Al<sub>2</sub>O<sub>3</sub>-based cermets and ensure the quality of final product.

In the present work, Al<sub>2</sub>O<sub>3</sub>–Co and Al<sub>2</sub>O<sub>3</sub>–(Co–50Ni) cermets were prepared by combustion synthesis in thermal explosion mode. The research focuses on preparing process, microstructures, and magnetic properties of cermets.

## Experimental methods

The reactions used to prepare Al<sub>2</sub>O<sub>3</sub>-based cermets were shown as follows:



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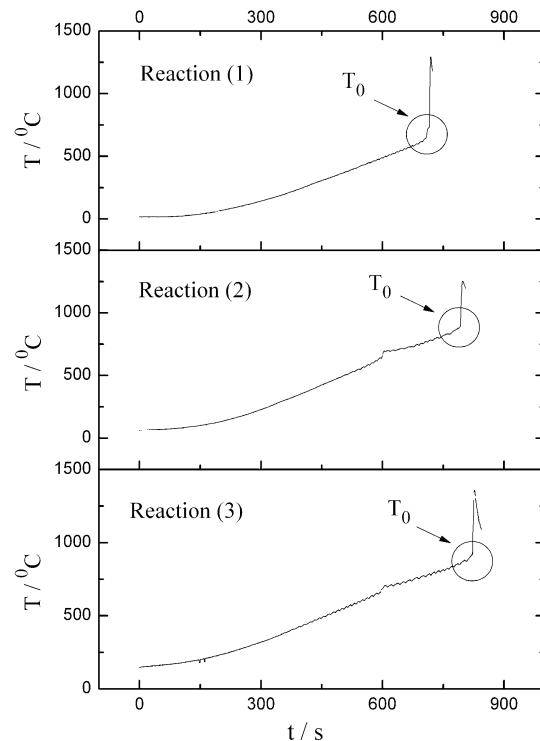
27.8 wt.% Co–Al<sub>2</sub>O<sub>3</sub> and 34.1 wt.% (Co–50Ni)–Al<sub>2</sub>O<sub>3</sub> cermets can be prepared by reaction (1) and reaction (2), respectively, where Al<sub>2</sub>O<sub>3</sub> plays the role of diluents. Meanwhile, we directly add pure Ni powder to form Co–50Ni alloy in reaction (3) in purpose of increasing the mass percentage of the metallic phase to about 45.2 wt.%.

Powders of Al, NiO, Co<sub>2</sub>O<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub>, and Ni ( $\geq 99\%$  purity) used in the experiments with average particle size less than 80  $\mu\text{m}$  as shown in Fig. 1a were originally supplied by SCRC (Sinopharm Chemical Reagent Co. Ltd, PR China). The mixture powders were prepared to get an average particle size of  $\sim 1.56 \mu\text{m}$  by ball milling in alcohol for 8 h as shown in Fig. 1b, then dried and pressed into compacts of  $\Phi 20 \times 10 \text{ mm}$  cylinder with 60% theoretical maximum density (TMD). The green compacts were heated in graphite crucible until the reaction was ignited, and the ignition temperature ( $T_0$ ) was detected by thermocouple put into the middle of the compact. The cermets were immediately densified by uniaxial loading ( $\sim 1.28 \text{ MPa}$ ) at the time of ignition, and the densities of cermets were measured based on Archimedes principle in alcohol. The microstructure and phase composition of cermets were characterized employing X-ray diffraction (XD-3A, SHIMADZU, USA) with Cr K $\alpha$  radiation (operating at 40 kV and 2°/min) and Sirion Field-emission Scanning Electron Microscope (FEI, Holland) with energy dispersive spectroscopy (EDS). The magnetic hystereses (M–H) of cermets were measured at room temperature using a Quantum Design (USA) vibrating sample magnetometer (VSM) in Physical Property Measurement System (PPMS-9).

## Results and discussion

### Reaction process

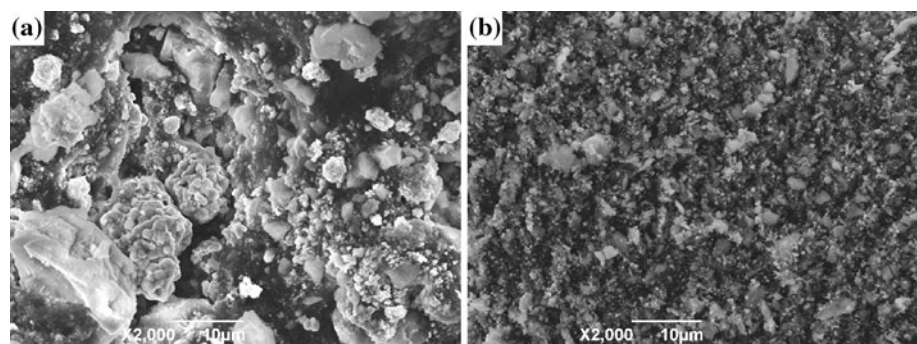
The green compacts are heated from room temperature to ignition temperature ( $T_0$ ) with the average heating rate of 1.32 °C/s. The temperature evaluation curves as shown in Fig. 2 indicate that  $T_0$  of reaction (1) is about 730 °C,



**Fig. 2** Temperature evolution curves of all reactions

which is much lower than that of reaction (2) ( $\sim 892 \text{ }^\circ\text{C}$ ) and reaction (3) ( $\sim 919 \text{ }^\circ\text{C}$ ). The reasons of such differences are as follows:  $T_0$  of 730 °C in reaction (1) indicates the ignition of Al–Co<sub>2</sub>O<sub>3</sub> reaction system; the higher  $T_0$  of 892 °C in reaction (2) is due to the simultaneous ignition of Al–Co<sub>2</sub>O<sub>3</sub> and Al–NiO systems that needs more energy supplying; in reaction (3), Ni powder, which is added into the compact in purpose of forming Co–50Ni alloy, plays the role of diluents rather than the reactants, so that  $T_0$  also increases. Subsequently, the rapid vertical raise of the temperature curves of all reactions indicates that the thermal explosion reaction occurs. At this moment, the production of dense cermets can be accomplished by applying uniaxial loading when the products are still hot and ductile. The relative densities of all synthesized cermets are shown in Table 1.

**Fig. 1** The morphology of mixture powders (a before ball milling, b after ball milling)



**Table 1** Density data of products

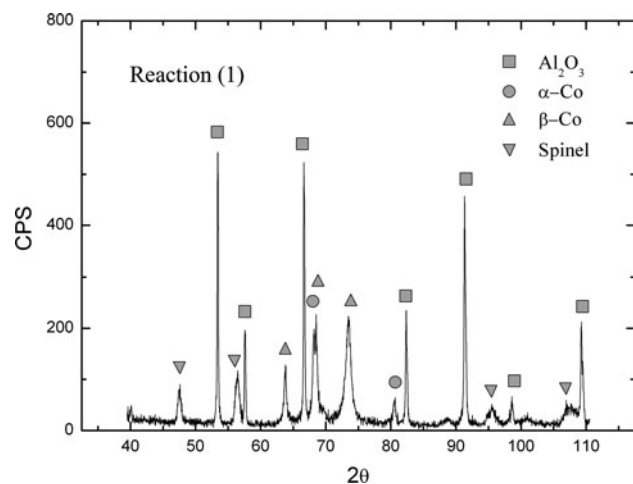
Reaction	Theoretical density/g/cm <sup>3</sup>	Measured density/g/cm <sup>3</sup>	Relative density/%
(1)	4.52	4.32	95.5
(2)	4.39	4.23	96.3
(3)	5.06	4.81	95

Phases and microstructures

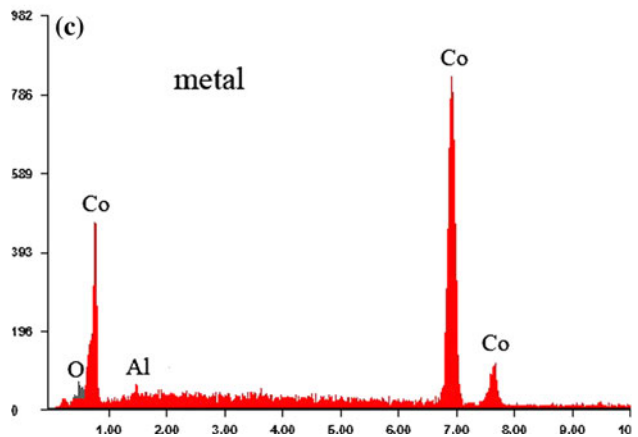
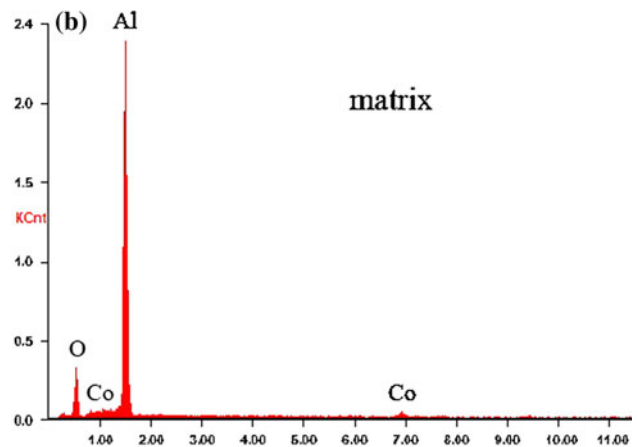
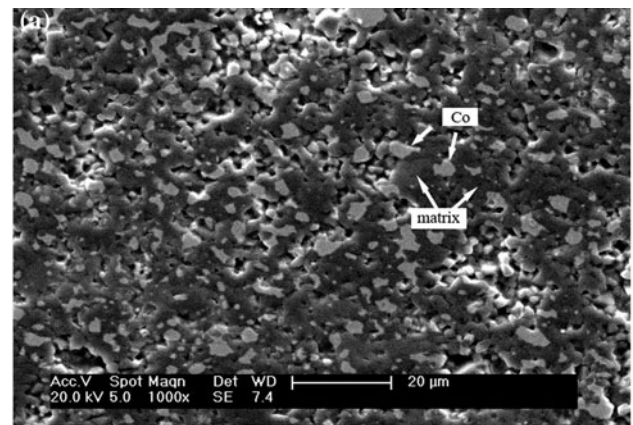
*Al<sub>2</sub>O<sub>3</sub>-Co cermets*

The XRD pattern for the cermets synthesized by reaction (1) as shown in Fig. 3 shows that Al<sub>2</sub>O<sub>3</sub> matrix and Co metal are obtained by thermite reaction, and the peaks of unreacted Al or Co-Al alloys are not found, that is, Al<sub>2</sub>O<sub>3</sub>-Co cermets are successfully prepared. Meanwhile, two kinds of allotropic Co phases are both found in the cermets. Prior work has found that the strain (or stress) plays the significant role in the allotropic transformation from β-Co to α-Co [11]. Therefore, high-temperature stable β-Co is firstly synthesized in combustion reaction [12] and then during the cooling stage, a part of β-Co particles are preserved by rapid heat loss through graphite crucible and the others are transformed to α-Co due to the inner heat stress of cermets. The XRD result also shows that the unexpected CoAl<sub>2</sub>O<sub>4</sub> spinel phases exist in the cermets.

Figure 4 shows the microstructure and EDS data of Al<sub>2</sub>O<sub>3</sub>-Co cermets. The intending Co particles with average size of less than 10 μm disperse homogeneously in the Al<sub>2</sub>O<sub>3</sub> matrix with solid solution of spinel phases. The approximate sphere Co particles are formed by the in-situ synthesized liquid Co agglomerating from adjacent region under high reaction temperature. However, the bulk agglomerated Co particles are not found because of Al<sub>2</sub>O<sub>3</sub>



**Fig. 3** XRD pattern for Al<sub>2</sub>O<sub>3</sub>-Co cermets

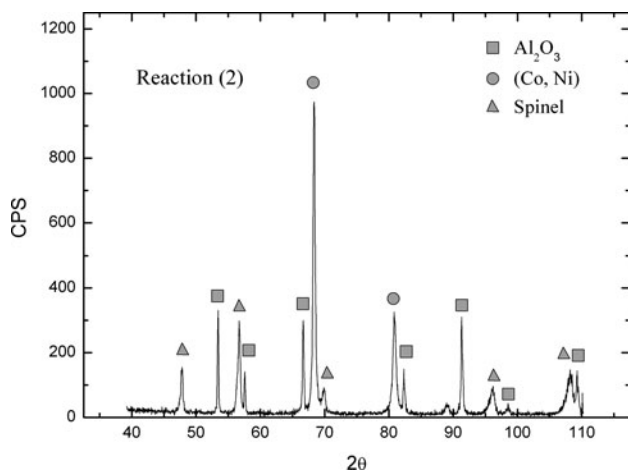


**Fig. 4** SEM micrograph and EDS data for Al<sub>2</sub>O<sub>3</sub>-Co cermets

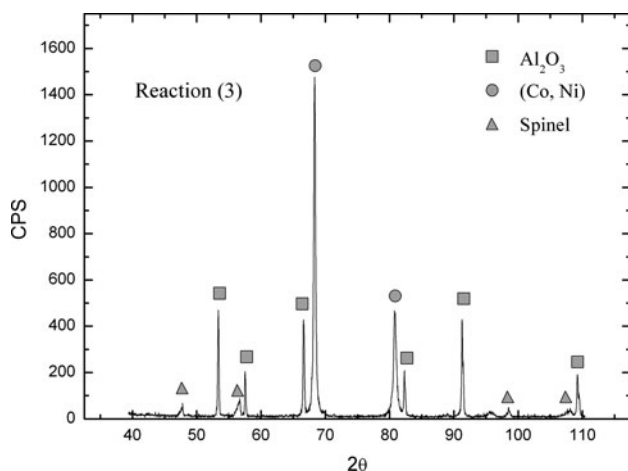
diluents absorbing a part of reaction heat and of the rapid heat loss after reaction. Meanwhile, most pores of the cermets after reaction are filled up by hot and ductile products when the uniaxial loading is applied, but a small amount of residual micro-pores still exist in the matrix because the separate micro-pores formed by the residual gas in the green compacts and by the volume shrinkage during cooling process are not entirely eliminated under this condition.

### $Al_2O_3$ –(Co–50Ni) cermets

In addition to synthesis of  $Al_2O_3$ –Co cermets (reaction (1)), we use Al–NiO system (reaction (2)) and Ni powders (reaction (3)) combined with Al–CoO system to prepare  $Al_2O_3$ –(Co–50Ni) cermets. The XRD patterns for both reactions as shown in Figs. 5 and 6, respectively, indicate that Co–50Ni alloys are well synthesized and the peaks of unreacted Al, Co–Al, or Ni–Al alloys are not found. Meanwhile, the peaks of unexpected (Co, Ni) $Al_2O_4$  spinel phases are found in both XRD results. In synthesis process, the spinel phase formed by CoO and NiO with  $Al_2O_3$  acts as an intermediate and then it reacts with residual liquid Al to form  $Al_2O_3$  and Co–50Ni alloy at high temperature during the reaction. However, Ni $Al_2O_4$  is difficult to be formed in reaction (3) due to Ni powders which cannot



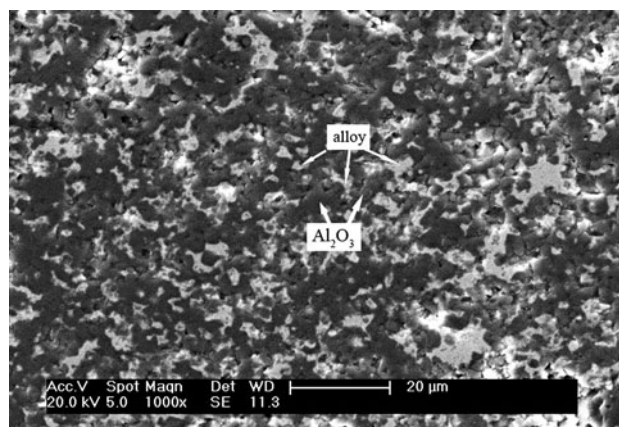
**Fig. 5** XRD pattern for  $Al_2O_3$ –(Co–50Ni) cermets fabricated by reaction (2)



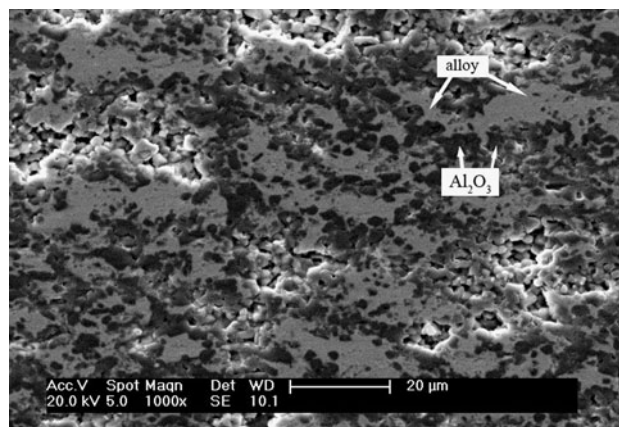
**Fig. 6** XRD pattern for  $Al_2O_3$ –(Co–50Ni) cermets fabricated by reaction (3)

directly react with  $Al_2O_3$  that explains the reduced intensity of spinel peaks.

Figures 7 and 8 show the microstructures of  $Al_2O_3$ –(Co–50Ni) cermets prepared by reaction (2) and reaction (3), respectively. The morphology of Co–50Ni particle is apparently different with that of Co particle in  $Al_2O_3$ –Co cermets. The network-like Co–50Ni alloy particles as shown in Fig. 7 distribute along the boundary of  $Al_2O_3$  particles. Moreover, a part of  $Al_2O_3$  particles are wrapped by the interpenetrating Co–50Ni alloys as shown in Fig. 8 when we increase the content of alloys, that is, the residual micro-pores and the boundary gaps of  $Al_2O_3$  particles can be filled up and the relative density of cermets can be improved. Therefore, we consider that the synthesized liquid Co–50Ni alloys can spread out on the surface of solid  $Al_2O_3$  particles, and then due to the effect of pressure, the alloys are squeezed by surrounding  $Al_2O_3$  particles and



**Fig. 7** SEM micrograph of  $Al_2O_3$ –(Co–50Ni) cermets fabricated by reaction (2)



**Fig. 8** SEM micrograph of  $Al_2O_3$ –(Co–50Ni) cermets fabricated by reaction (3)



finally can infiltrate into the boundary gaps to form network-like morphology during the cooling stage.

Magnetic properties

The magnetic hysteresis (M–H) loops of the cermet as shown in Figs. 9, 10, and 11, respectively, indicate that  $\text{Al}_2\text{O}_3\text{–Co}$  and  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  cermets are all ferromagnetic. Since  $\text{Al}_2\text{O}_3$  is non-magnetic, the magnetic properties of cermets strongly depend on the magnetic Co and Co–50Ni phases. The parameters related to magnetic properties are summarized in Table 2. The lower saturation magnetization of  $\text{Al}_2\text{O}_3\text{–Co}$  cermets, which is about 42 emu/g and achieved for applied magnetic field that are above a value of 10 kOe or below a value of  $-10$  kOe, is due to the  $\beta\text{-Co}$  preserved in the matrix which only presents magnetic property over 1121 °C. With incorporation of Ni, the saturation magnetizations of two kinds of  $\text{Al}_2\text{O}_3\text{–}$

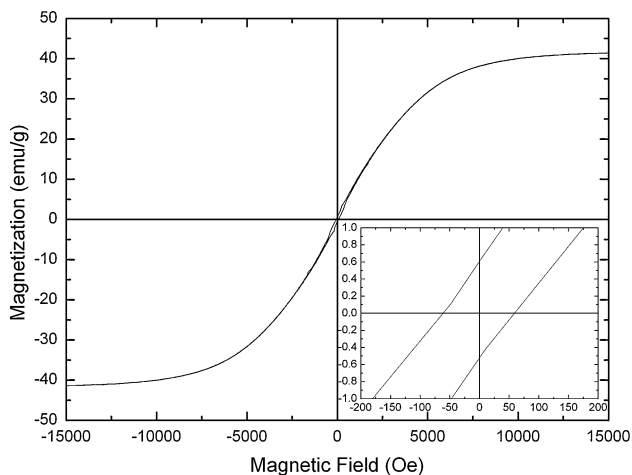


Fig. 9 The magnetic hysteresis (M–H) loops of  $\text{Al}_2\text{O}_3\text{–Co}$  cermets

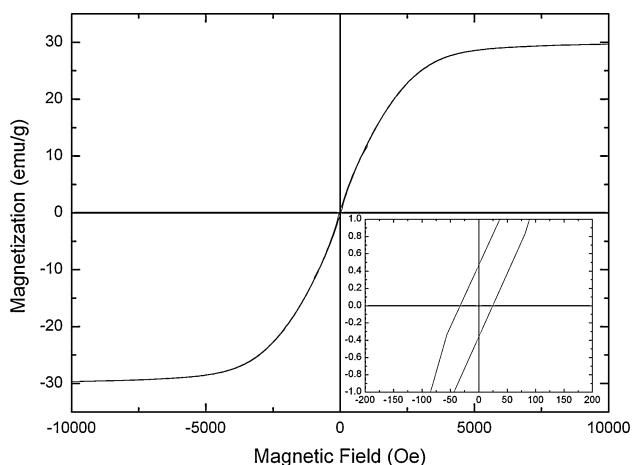


Fig. 10 The magnetic hysteresis (M–H) loops of  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  fabricated by reaction (2)

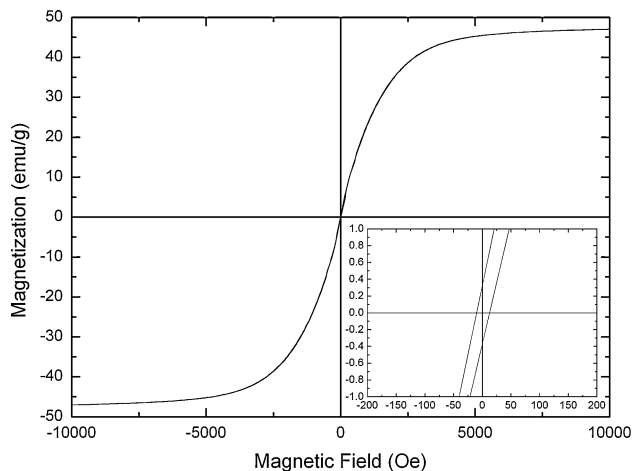


Fig. 11 The magnetic hysteresis (M–H) loops of  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  fabricated by reaction (3)

(Co–50Ni) cermets are achieved for applied much lower magnetic fields. We consider that  $\text{Al}_2\text{O}_3\text{–Co}$  cermet is a kind of semi-hard magnetic composites, but  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  cermets represent soft magnetic property. Meanwhile, the saturation magnetization of  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  prepared by reaction (2) decreases to about 30 emu/g because the saturation magnetization of Co–50Ni alloy is lower than that of Co metal and more spinel phases are synthesized in the matrix. However, when we increase the content of magnetic Co–50Ni alloys in reaction (3), the saturation magnetization of  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  increases to about 48 emu/g.

The coercive force is known to depend on the magnetic properties of the magnetic phases and on the grain size, residual stress, and dislocation density of the cermets [7]. The micro-scale Co–50Ni particles which represent soft magnetic property lead to the decrease of coercive force in  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  cermets. Moreover, the coercive force of the cermets prepared by reaction (3) further decreases to 11.17 Oe since the Co–50Ni particles become larger due to agglomeration and coalition when its content increases. We expect that nano-scale magnetic particles leading to a high coercive force can be prepared by this method in future study, for when the particle size of a magnetic material decreases, its magnetic structure varies from a multidomain state to a single-domain state, to reduce the total energy of the system [7]. In summary, the ferromagnetic Co–50Ni alloys are responsible of high magnetic susceptibility and low coercive force of  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  cermets.

Summary and conclusions

The ferromagnetic  $\text{Al}_2\text{O}_3\text{–Co}$  and  $\text{Al}_2\text{O}_3\text{–(Co–50Ni)}$  cermets were successfully prepared by combustion synthesis

**Table 2** The parameters related to the magnetic properties

Cermets	Reactants	Saturation magnetization (emu/g)	Coercive force (Oe)
Al <sub>2</sub> O <sub>3</sub> -Co	Al-Co <sub>2</sub> O <sub>3</sub> -Al <sub>2</sub> O <sub>3</sub>	41.84	60.86
Al <sub>2</sub> O <sub>3</sub> -(Co-50Ni)	Al-Co <sub>2</sub> O <sub>3</sub> -NiO-Al <sub>2</sub> O <sub>3</sub>	29.96	28.48
Al <sub>2</sub> O <sub>3</sub> -(Co-50Ni)	Al-Co <sub>2</sub> O <sub>3</sub> -Ni-Al <sub>2</sub> O <sub>3</sub>	47.59	11.17

in thermal explosion mode. The production of dense cermets (relative density >95%) can be accomplished via uniaxial loading (about 1.28 MPa).

In Al<sub>2</sub>O<sub>3</sub>-Co cermets, in-situ synthesized Co particles disperse homogeneously in the matrix where  $\beta$ -Co and  $\alpha$ -Co co-exist at room temperature. However, the shape of Co-50Ni alloy particle synthesized by Al-CoO system either with Al-NiO system or with direct adding of Ni powder becomes irregular and the alloys can infiltrate into the boundary of Al<sub>2</sub>O<sub>3</sub> particles. Meanwhile, all of the cermets have a small quantity of residual spinel phases.

The analysis of magnetic properties shows that the saturation magnetization of Al<sub>2</sub>O<sub>3</sub>-based cermets strongly depends on the magnetic characteristic and ratios of Co and Co-50Ni. The ferromagnetic Co-50Ni alloys are responsible of high magnetic susceptibility and low coercive force of Al<sub>2</sub>O<sub>3</sub>-(Co-50Ni) cermets.

**Acknowledgements** An acknowledgement is due to associate professors Fan Li and Haibo Huang for the SEM facility and associate

professor Xun Xiao for the XRD facility in Analysis and Testing Center of SEU. The authors also would like to thank to Mr. Xun Dong and Mr. Yancheng Zhang for the valuable discussions in the experiments.

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